

# Surface interaction of H<sub>2</sub>O and O<sub>2</sub> on the ternary Fe<sub>1-x</sub>X<sub>x</sub>Al metal alloy doped with Ru and Pd

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**Abstract.** Surface interaction is one of the most frequently utilized computational techniques for atomistic simulation and describing point defects in solid-state materials. The surface energy (energy of pure system)/or surface free energy (energy of the system with adsorbent) quantifies the disruption of intermolecular bonds when a surface is adsorbed on the ternary adsorbate Fe<sub>1-x</sub>X<sub>x</sub>Al. Typical surface properties such as adsorption, adhesion, weather resistance, corrosion resistance, and chemical resistance contribute to determining the stability of materials. The current study has explored the surface adsorption of H<sub>2</sub>O and O<sub>2</sub> on the Fe<sub>1-x</sub>X<sub>x</sub>Al ternary system to address the challenge of corrosion and oxidation effects. In particular, the surface interaction is investigated to cleave surface models by observing point defects of terminations to determine the bonding strength that can resist the oxidation process. The E<sub>ads</sub>/H<sub>2</sub>O showed higher energies compared to those of O<sub>2</sub>, which implies that E<sub>ads</sub>/O<sub>2</sub> is more stable with the lowest energies compared to those of H<sub>2</sub>O.

## 1 Introduction

Surface interaction has allowed a broader spectrum to investigate and mitigate the challenges of oxidation for the development of solid-state materials, leading to improved component coating in stainless-steel and cost-effective production. Reactions on types of coating on the surfaces have been conducted by Fones and Hatton using computer simulations [1]. Their equilibrium structures (Wulff shape) were based on the Wulff cluster model. This model was proved preliminarily by calculating the concentration trend of Al/Fe atoms on both Al-terminated and Fe-terminated surfaces, and by simulating the most stable layer adsorbed on these two surfaces. It was reported that environmental moisture-induced and temperature are leading causes of low tensile ductility and brittle cleavage fracture on the Fe-rich FeAl alloy. This results in deformation, fracture on the design of the β2 iron aluminide-based alloy, and poor yield-strength anomaly at intermediate temperature. However, possible cracks can be observed on the surface of the system if the surface yields low free surface energy contributing to fracture effects. Thus, there is still a need to explore the corrosion and oxidation behavior in order to increase adhesion, and capacity to tolerate creep resistance [2,

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3]. In general, iron-aluminides are reported to show a major embrittlement mechanism at room temperature, resulting in a loss of cohesive strength at their interfaces [4].

On the other hand, intermetallic alloys exhibit unique surface properties, including high hardness, good wear and corrosion resistance, and the ability to form adherent surface oxides, making them suitable for applications for high-temperature structural components and coatings [5]. In order to understand the behaviour and interaction of the intermetallic, various surface terminations are considered. This is done by cleaving the most stable slab model, which will allow doping on the surface and adsorption. This provides valuable insight into the binding capacity, bonding strength and adhesion abilities, resulting in a reduction to surface oxidation. However, the strength of the material can be negatively influenced by environmental effects such as hazardous chemicals in the atmosphere, moisture, and heat, which may have the ability to deteriorate the mechanical properties. Mkhonto *et al.* A molecular dynamics study of  $\text{Fe}_{50-x}\text{M}_x\text{Al}_{50}$  ternary alloy (M=Ag, Pt, Pd) in 2020, the intermetallic studies on the mechanical and dynamical properties of  $\text{Fe}_{1-x}\text{X}_x\text{Al}$  (X = Pt and Ru) Alloys, in 2022, the effect of alloying on  $\beta$ 2-ordered FeAl with Pd and Ir for high-temperature application and ductility enhancement in 2023. This is to determine the effect of ternary alloying under various conditions to enhance the stability of iron aluminides [6, 7, 8]

It is crucial to consider factors affecting adhesion, durability, creep resistance, oxidation and ductility of the surface when exposed to various conditions for specific tailored applications in automotive parts, turbines, in particular, in aerospace infrastructures. The aluminides have remarkably become the most applied coating method in protective coatings because they possess excellent high-temperature corrosion resistance [9]. Maintaining aluminium content is favorable, and the adhesion scale to the substrate is a protective barrier, guaranteeing intermetallic alloys that are corrosion resistant [10, 11]. This study demonstrated that doping the pristine FeAl with Ru and Pd greatly improved its surface stability. Determining the surface interaction of  $\text{H}_2\text{O}$  and  $\text{O}_2$  demonstrated the impact it has on the  $\text{F}_{1-x}\text{X}_x\text{Al}$  ternary system after improving the stability of the system through adsorption a third metal on the pristine FeAl alloys.

## 2 Methodology

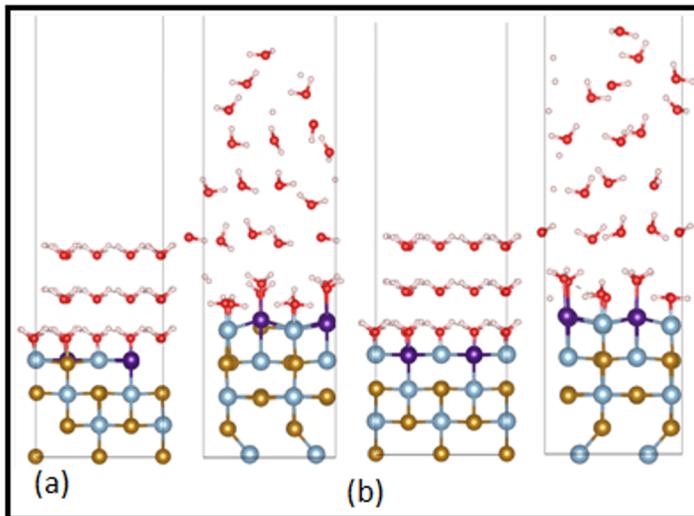
Computational modelling techniques such as VASP and CASTEP were employed to determine the surface stability of  $\text{Fe}_{1-x}\text{Ru}_x/\text{Pd}_x\text{Al}$  systems. We have employed the first-principles DFT [12] method to determine the surface adsorption and bond strength of the ternary  $\text{F}_{1-x}\text{X}_x\text{Al}$  system. The Perdew-Berke-Ernzerhof (PBE) [13] functional and generalized gradient approximation (GGA) [14] for estimating calculations were employed. Moreover, a plane-wave pseudopotential functional [15] with a cut-off energy of 270 eV was sufficient to allow the systems to converge. METADISE code [16], was used to cleave the conventional (110) surface plane of the pristine FeAl system. VESTA-win64 was also used to visualize crystal structures and three-dimensional data, including the volumetric data and crystal morphologies of the  $\text{F}_{1-x}\text{X}_x\text{Al}$  system [17]. This is followed by cleaving slab models on the (110) surface plane in order to identify the suitable slab with the lowest surface energy for the design of ternary  $\text{Fe}_{1-x}\text{X}_x\text{Al}$  systems by adsorbing a third element Ru and Pd to enhance surface stability which will be identified as surface free energy. Further calculations were done by determining the interaction of  $\text{H}_2\text{O}$  and  $\text{O}_2$  on the ternary  $\text{F}_{1-x}\text{X}_x\text{Al}$  system.

## 3 Results and discussion

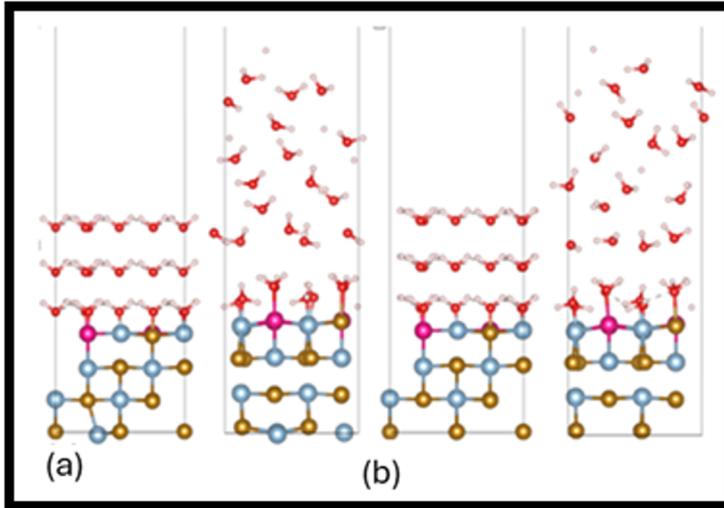
### 3.1 H<sub>2</sub>O interaction on Fe<sub>1-x</sub>Y<sub>x</sub>Al system

In this section, we have carried out density functional theory calculations with long-range dispersion corrections to investigate the interaction of H<sub>2</sub>O and O<sub>2</sub> on the most stable Fe<sub>1-x</sub>X<sub>x</sub>Al (110) surfaces. This is done in order to determine the surface energies of the most stable site with different concentrations of X element. Ru and Pd are both platinum group metals with diverse properties and applications. Herein, Ru is a chosen adsorbent due to its hard, high boiling and melting point and does not tarnish at room temperature. Where else Pd is malleable and ductile. These adsorbents have the potential to enhance durability, increase oxidation and corrosion resistance of the pristine FeAl system. Thus, the introduction of H<sub>2</sub>O and O<sub>2</sub> adsorption is to observe the effect as these materials will be exposed to various environmental conditions.

Figure 1 to Figure 2 illustrate adsorption of H<sub>2</sub>O on the ternary Fe<sub>1-x</sub>Ru<sub>x</sub>Al and Fe<sub>1-x</sub>Pd<sub>x</sub>Al systems, respectively. The pristine FeAl alloy is a potential structural material especially when adsorbed with Ru/Pd adsorbents to enhance the strength and surface stability. Therein, there is a need to observe the interaction of H<sub>2</sub>O on the Fe<sub>1-x</sub>Ru<sub>x</sub>Al and Fe<sub>1-x</sub>Pd<sub>x</sub>Al systems. This reaction has been known to have a negative effect on surface properties. These models were chosen due usage of METADISE code which cleaves slab models with zero dipole moment, that is, symmetrical shape, causing the bond of dipoles and in turn improving their physical properties, such as boiling point.



**Fig. 1.** Adsorption of H<sub>2</sub>O on ternary Fe<sub>1-x</sub>X<sub>x</sub>Al on (110) surface; brown- Fe, light blue- Al, dark blue representing the adsorbent Ru.



**Fig. 2.** Adsorption of H<sub>2</sub>O on ternary Fe<sub>1-x</sub>X<sub>x</sub>Al on (110) surface; brown- Fe, light blue- Al, pink representing the adsorbent Pd.

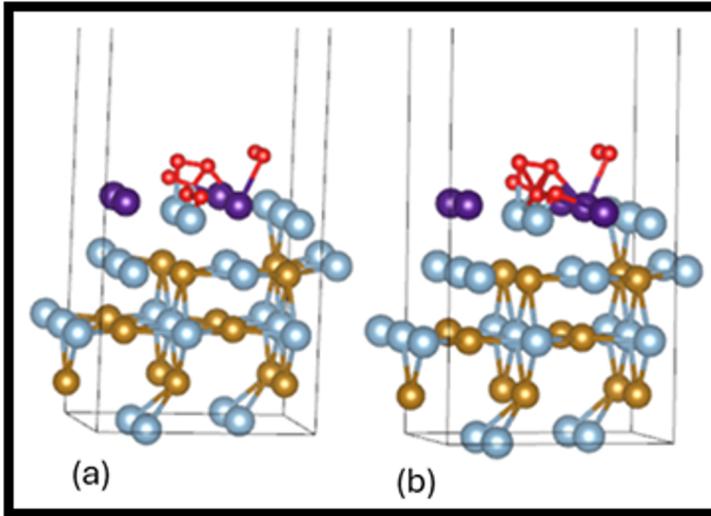
The concentrations were varied from 1 to 4 on each slab since higher concentrations destabilize the systems, leading to brittleness and an increase in oxidation. The most stable slab models with doped concentrations from 1\_Pd/Ru up to 4\_Pd/Ru were chosen. During the adsorption of H<sub>2</sub>O molecules on various ternary Fe<sub>1-x</sub>X<sub>x</sub>Al surfaces, the results show that the lowest adsorption energy was obtained from 2\_Pd, followed by 2\_Ru and 4\_Ru as the least stable, with values of 8.116, 8.234, and 8.305 J m<sup>-2</sup>, respectively. When the surface coverage was increased up to a monolayer, we noted an increase in E<sub>ads</sub>/H<sub>2</sub>O with increasing coverage for the Fe<sub>1-x</sub>X<sub>x</sub>Al surface, resulting in instability.

**Table 1.** The adsorption energy of H<sub>2</sub>O on the stable site of each ternary Fe<sub>1-x</sub>Y<sub>x</sub>Al system illustrating the surface free energy (SFE), Energy of modified (E<sub>mod</sub>) system, energy of Iron (E<sub>Fe</sub>), energy of the pristine (E<sub>Prist</sub>), energy of the adsorbent (E<sub>X</sub>) and adsorption energy (E<sub>ads</sub>).

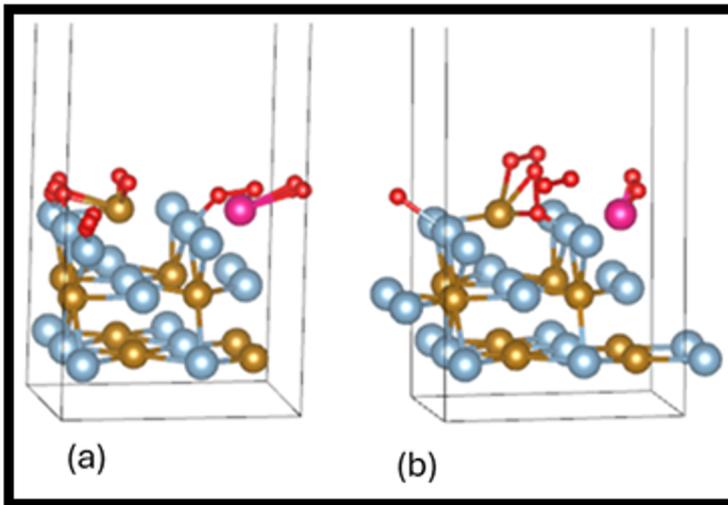
Concentration	SFE (J m <sup>-2</sup> )	E <sub>mod</sub> (J m <sup>-2</sup> )	E <sub>Fe</sub> (J m <sup>-2</sup> )	E <sub>prist</sub> (J m <sup>-2</sup> )	E <sub>X</sub> (J m <sup>-2</sup> )	E <sub>X</sub> /atom (J m <sup>-2</sup> )	E <sub>ads</sub> /H <sub>2</sub> O (J m <sup>-2</sup> )
2_Pd	0.165	-553.663	-4.99	-187.90	-5.21	-1.30	8.116
2_Ru	0.165	-559.174	-4.99	-187.90	-2.72	-1.36	8.234
4_Ru	0.165	-562.499	-4.99	-187.90	-2.72	-1.36	8.305

### 3.2 O<sub>2</sub> interaction on Fe<sub>1-x</sub>Y<sub>x</sub>Al system

Figures 3 and 4 show how oxygen chemisorbs onto the ternary Fe<sub>1-x</sub>Y<sub>x</sub>Al alloy. It has been demonstrated that O<sub>2</sub> reactions improve surface stability through the formation of an oxide layer (Al<sub>2</sub>O<sub>3</sub> [18, 19]).



**Fig. 3.** Adsorption of O<sub>2</sub> bridge on ternary Fe<sub>1-x</sub>X<sub>x</sub>Al on (110) surface; brown- Fe, light blue- Al, dark blue representing the adsorbent Ru.



**Fig. 4.** Adsorption of O<sub>2</sub> mono on ternary Fe<sub>1-x</sub>X<sub>x</sub>Al on (110) surface; brown- Fe, light blue- Al, pink representing the adsorbent Pd.

The O<sub>2</sub> molecule was adsorbed on the ternary Fe<sub>1-x</sub>X<sub>x</sub>Al system as mono and bridge in order to evaluate the surface energies. To obtain accuracy between the nuclei of two bonded atoms. This is based on data from crystal structures of various complexes. The results indicate that 2\_Pd\_mono had the lowest adsorption energy, followed by 2\_Pd\_bridge, 4\_Ru\_mono and 4\_Ru\_bridge as the least stable with values of 0.794, 0.889, 1.081 and 1.191 J m<sup>-2</sup>, respectively. When O<sub>2</sub> was adsorbed on the surface of Fe<sub>1-x</sub>X<sub>x</sub>Al, the adsorption energy was lower compared to the adsorption of H<sub>2</sub>O.

**Table 2.** Adsorption energy of O<sub>2</sub> on the stable site of each ternary Fe<sub>1-x</sub>X<sub>x</sub>Al system, indicating the surface free energy (SFE), Energy of modified (E<sub>mod</sub>) system, energy of Iron (E<sub>Fe</sub>), energy of the pristine (E<sub>Prist</sub>), energy of the adsorbent (E<sub>X</sub>), and the adsorption energy (E<sub>ads</sub>).

Concentrations	SFE (J m <sup>-2</sup> )	E <sub>mod</sub> (J m <sup>-2</sup> )	E <sub>Fe</sub> (J m <sup>-2</sup> )	E <sub>prist</sub> (J m <sup>-2</sup> )	E <sub>X</sub> (J m <sup>-2</sup> )	E <sub>X</sub> /atom (J m <sup>-2</sup> )	E <sub>ads</sub> /O <sub>2</sub> (J m <sup>-2</sup> )
2_Pd_Mono	0.165	-213.448	-4.99	-187.90	-5.210	-1.303	0.794
2_Pd_Bridge	0.165	-217.868	-4.99	-187.90	-5.210	-1.303	0.889
4_Ru_Mono	0.165	-226.853	-4.99	-187.90	-2.723	-1.362	1.081
4_Ru_Bridge	0.165	-231.978	-4.99	-187.90	-2.723	-1.362	1.191

## 4 Conclusion

The interaction of O<sub>2</sub> and H<sub>2</sub>O on the Fe<sub>1-x</sub>X<sub>x</sub>Al surface was successfully deduced from surface free energy and adsorption energy calculations using DFT. The behaviour of E<sub>ads</sub>/H<sub>2</sub>O showed higher surface energies compared to those of E<sub>ads</sub>/O<sub>2</sub>, which illustrated that E<sub>ads</sub>/O<sub>2</sub> is more stable with the lower energies. The oxide layer (Al<sub>2</sub>O<sub>3</sub>) formed through the interaction of Al and O<sub>2</sub>, which increases corrosion resistance necessary regardless of the production processes. The deterioration on the surfaces of metals would result in increased oxidation process, pressing demand for more resources, implying high costs of production. This behaviour leads to chemical occurrence on the surface of the material, in particular, how oxidation affects the durability of the Fe<sub>1-x</sub>X<sub>x</sub>Al system, resulting in corrosion. As the metal reacts with the environment, it causes a redox reaction and the deterioration of steel, which is not visible to the naked eye. Hence, the study of surface stability assisted in determining the best process to identify how a protective oxide layer can be formed for component coating for superior protection. The adsorption of O<sub>2</sub> on the surface of the ternary system contributed to the formation of the oxide layer compared to the adsorption of H<sub>2</sub>O.

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## References

1. A. Fones and G. Hatton, Effects of Platinum Group Metals Doping on stainless steel. *Platn. Met. Rev.* **58**, 1 (2014).  
<https://doi.org/10.1595/147106714X676640>
2. C. T. Liu, E. P. George, P. J. Maziasz and J. H. Schneibel, Recent advances in B2 iron aluminide alloys: Deformation, fracture and alloy design. *Mater. Sci. Eng. A* **258**, 1-2 (1998).  
[https://doi.org/10.1016/S0921-5093\(98\)00921-6](https://doi.org/10.1016/S0921-5093(98)00921-6)

3. J. Cebulski, D. Pasek, M. Bik, K. Świerczek, P. Jeleń, K. Mroczka, J. Dąbrowa, M. Zajusz, J. Wyrwa and M. Sitarz, In-situ XRD investigations of FeAl intermetallic phase-based alloy oxidation, *Corros. Sci.* **164**, 108344 (2020).  
<https://doi.org/10.1016/j.corsci.2019.108344>
4. B. M. Mutasa, *Defect Structures in Ordered Intermetallics; Grain Boundaries and Surfaces in FeAl, NiAl, CoAl and TiAl*, (Blacksburg, Virginia Polytechnic Institute and State University, 1997).
5. P. A. Mc Quay, V. K. Sikka, Y.E. Khalfalla and K.Y. Benyounis, Casting of Intermetallics, *Mater. Sci.* **6**, 2001 (2016).  
[doi:10.1016/B0-08-043152-6/00187-X](https://doi.org/10.1016/B0-08-043152-6/00187-X)
6. C. S. Mkhonto, N. L. Lethole, P. E. Ngoepe and H. R. Chauke, digital technology in production development, The 23rd Annual International Conference at the Hazendal wine estate in Stellenbosch, RAPDASA Conference, November 8 - 11 (2022).  
<https://doi.org/10.1051/mateconf/202237009006>
7. C. S. Mkhonto, P. E. Ngoepe and H. R. Chauke, in Proceedings of the MRS Advances-2020 conference, materials education/networking in materials science & engineering, Nelson Mandela African Institute for Science and Technology, in Arusha, Tanzania, from December 10 – 13, (2020).  
DOI: 10.1557/adv.2020.177
8. C. S. Mkhonto, P. E. Ngoepe and H. R. Chauke, Advanced Manufacturing Beyond Borders, The 24th Annual International Conference, CSIR International Convention Centre in Pretoria, 30 October - 02 November, (2023).  
<https://doi.org/10.1051/mateconf/202338802004>
9. G. Fu, Z. Qi, Y. Su, Q. Liu and X. Guo, Effect of Different Treatment on Corrosion, *High Temp. Mater.* **33**, 6 (2014).  
<https://doi.org/10.1515/htmp-2013-0110>
10. J. Cebulski, D. Pasek, M. Sozanska, M. Popczyk, J. Gabor and A. Swinarew, “Oxidation of the alloy based on the intermetallic phase FeAl in the temperature range of 700-1000oC in air and possibilities of practical application, *Mater.* **18**, 1835 (2025).  
<https://doi.org/10.3390/ma18081835>
11. Y. N. Mansurov and J. U. Rakhmonov, Analysis of the phase composition and the structure of aluminum alloys with increased content of impurities, *Mater. Sci.* **2** (2018).  
DOI: 10.17580/nfm.2018.02.07
12. A.E. Mattson, P.A. Schultz, M.P. Desjarlais, T.R. Mattsson and K. Leung, Designing meaningful density functional theory calculations in materials science, *Mod. and Simul. Mater. Sci. Eng.* **1** (2005).  
DOI 10.1088/0965-0393/13/1/R01
13. J.P. Perdew, K. Burke and M. Ernzerhof, Generalized gradient approximation made simple, *Phys. Rev. Lett.* **77**, 1396 (1996).  
<https://doi.org/10.1103/PhysRevLett.77.3865>
14. E. Matthias and J.P. Perdew, Generalized gradient approximation to the angle- and system-averaged exchange hole, *J. Chem. Phys.* **109**, 9 (1998).  
<https://doi.org/10.1063/1.476928>
15. G. Kresse and J. Furthmüller, Efficient iterative schemes for ab initio total-energy calculations using a plane-wave basis set, *Phys. Rev. B* **54**, 11169 (1996)  
<https://doi.org/10.1103/PhysRevB.54.11169>
16. G. W. Watson, E. T. Kelsey, N. H. de Leeuw, D. J. Harris and S. C. Parker, Faraday Transition Atomistic simulation of dislocations, surfaces and interfaces in MgO, *J. Chem. Soc.* **92**, 3 (1996).  
<https://doi.org/10.1039/FT9969200433>

17. M. J. Ungerer, D. Santos-Carballal, A. Cadi-Essadek, C. G. C. E. van Sittert, and N. H. de Leeuw, Interaction of H<sub>2</sub>O with the Platinum Pt (001), (011), and (111) Surfaces: A Density Functional Theory Study with Long-Range Dispersion Corrections, *J. Phys. Chem. C* **123**, 27466 (2019).

[https://doi: 10.1021/acs.jpcc.9b06136](https://doi.org/10.1021/acs.jpcc.9b06136)

18. P. G. Gonzales-Ormeno, H. M. Petrilli and C. G. Schon, Ab initio calculation of the bcc Fe-Al phase diagram including magnetic interactions, *Scripta Mater.* **54**, 7 (2006).

<https://doi.org/10.1016/j.scriptamat.2005.12.024>

19. K. M. Doleker, The Examination of Microstructure and Thermal Oxidation behaviour of laser-remelted high-velocity oxygen liquid fuel Fe/Al coating, *J. Mater. Eng. Perfor.* **29**, 5 (2020).

<https://doi.org/10.1007/s11665-020-04873-z>